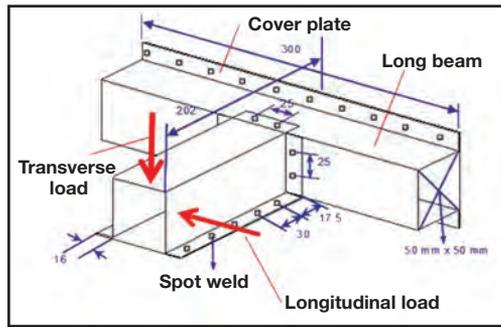


Fig. 2 — A component sample used to validate spot weld failure parameters.



ing samples to fixtures and eliminating slippage during testing. Holes were also added to the cover plate on the long beam of the T-section sample, to attach the plate to the fixture.

Small sample testing

Sample testing must be conducted with different strain rates because a spot weld's axial strength, shear strength, and bending strength is a function of strain rate as shown in Equation 1. Typically, three strain rate tests are conducted including static testing for low strain rate, intermediate speed testing for medium strain rate, and high-speed testing for high strain rate. Note that high-speed testing is more important than static testing because most crash impact testing is conducted at high speeds, such as 50 mph or higher.

Testing fixtures are designed to simulate the rigid conditions in automotive spot welded structures for small sample testing. Figures 4 and 5 show the testing fixture used for KSII-90°, KSII-60°, KSII-30°, KSII-0°, lap-shear, coach-peel, and torsional samples. The same testing fixtures are used for static, intermediate, and high-speed testing.

Both static and intermediate speed tests are performed with an electromechanical test system at a 50 mm/min and 50 mm/second crosshead speed, respectively. Sample displacement is measured using both an extensometer, as shown in Figs. 4 and 5, and the crosshead positioning system. Load is recorded by a load cell.

Figure 6 shows a typical *load vs. time* and *displacement vs. time* graph for a spot weld static test. Five tests were conducted for the same conditions to check data repeatability. Small variations resulting from weld size differences were found, and the peak load was used to determine spot weld joint strength for developing failure parameters. Load curve after peak load was used to determine damage parameters. Figure 7 shows broken samples for KSII, coach-peel, and lap-shear testing. KSII and coach-peel samples exhibit pullout-button failure, while the lap-shear sample shows interfacial failure.

High-speed tests were performed on a modified Dynatup Model 8250 (General Research Corp.) instrumented drop weight tower, shown in Fig. 8. Consistent with static tests, the same upper and lower sample holders using bolts

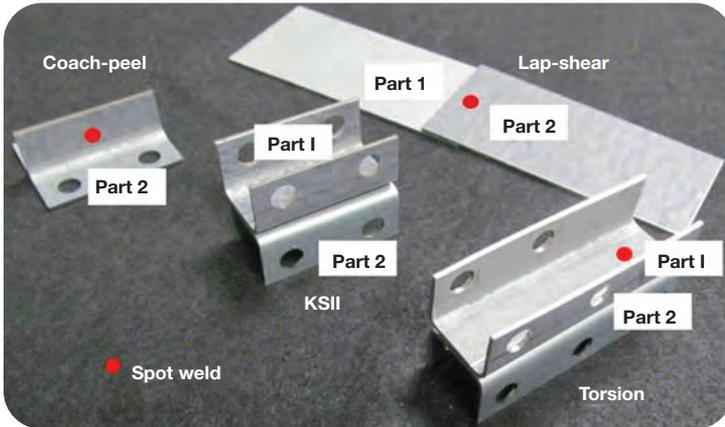


Fig. 3 — Welded versions of small samples.

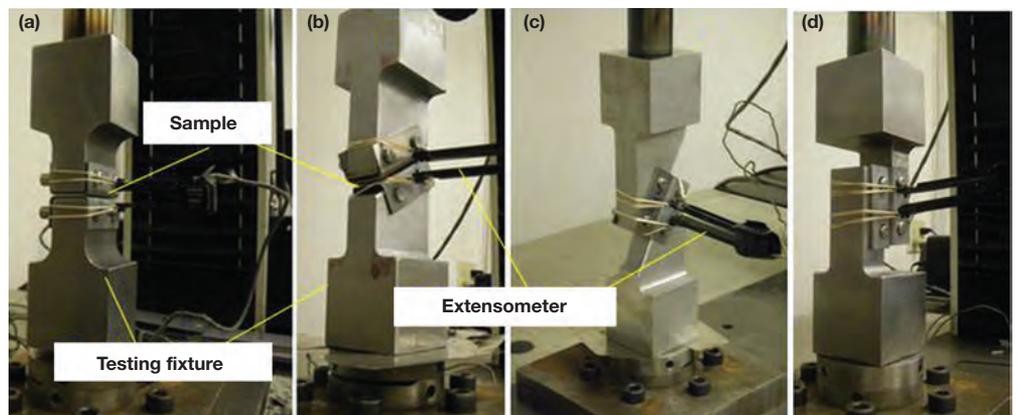
longitudinal load, respectively^[5]. Testing was modeled using finite element analysis (FEA) to predict spot weld failures by inputting the failure parameters developed from the small samples, and then comparing these with testing results to validate the spot weld failure parameters.

Sample fabrication

Sheet metal was cut and formed into the C-channel shape according to the dimensions shown in Fig. 1. Weld fixtures were designed to prepare the samples and welding procedures were supplied by the automotive manufacturer. Figure 3 shows the welded KSII, coach-peel, lap-shear, and torsional samples with one spot weld. Weld size could be either the minimum size (normally $4\sqrt{t}$, where t is the sheet thickness in mm) or the actual weld size used in the vehicle. If the minimum size is selected, the developed failure parameters will be conservative, which is preferred for automotive structure design.

Holes were drilled in samples prior to welding, for bolt-

Fig. 4 — KSII sample testing: (a) 90° loading, (b) 60° loading, (c) 30° loading, and (d) 0° loading.



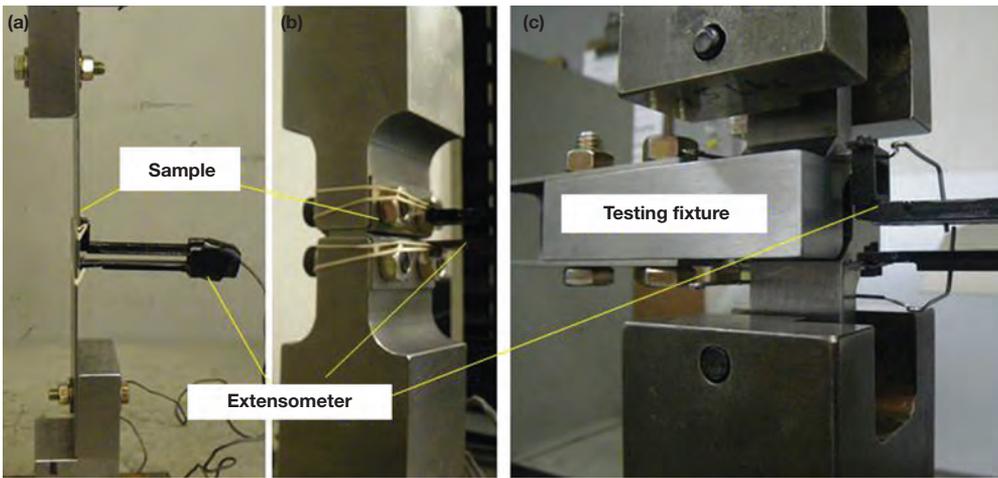


Fig. 5 — Testing of (a) lap-shear, (b) coach-peel, and (c) torsional samples.

or pin connections were used for high-speed testing. Impact load was measured at the reaction point during the impact event using a strain gauge-type load cell attached below the rigid table structure. The load cell was connected to the welded coupon through the upper sample holder. The moving head was dropped from a free-fall height of 2.59 m (8.5 ft). The moving mass contacted an impact bar extending through the structure and connected to the lower sample holder. Load was transmitted directly to the bottom attachment point of the test coupon. Sample displacement was measured using a linear voltage displacement transducer (LVDT) placed between sample attachment points.

T-section sample testing

Longitudinal and transverse loading were applied during T-section sample testing, as illustrated in Fig. 2. T-section static testing was conducted with an electromechanical test system and a fixture was designed to rigidly secure the T-section sample during testing. The fixture includes a 45 × 45-mm backing bar inside the long beam to bolt the sample to the fixture base through the holes in the cover plate (Fig. 2).

High-speed testing was conducted using an MTS drop tower, instrumented with an LVDT and load cells. The same rigid test fixture used for the static tests was used in the high-speed testing. Figure 9 shows broken T-samples for transverse and longitudinal loading. For transverse loading, spot welds were broken at the cover plate joined to the long beam. For longitudinal loading, spot welds were broken at the long beam to short beam intersection. FEA was conducted using the failure parameters developed from the small samples to predict spot weld failure and validate the final failure parameters.

Summary

A test method was developed to create spot weld failure parameters (joint strength at axial, shear, torsional, and combined loading) for crash simulation during automotive structure design. The method includes testing small samples and T-section samples. Small samples consisting of KSII, lap-shear, coach-peel, and torsional configurations were designed to evaluate the axial, shear, and bending strength of spot welds, as well as the strength during combined axial, shear, and bending loads. T-section samples were de-

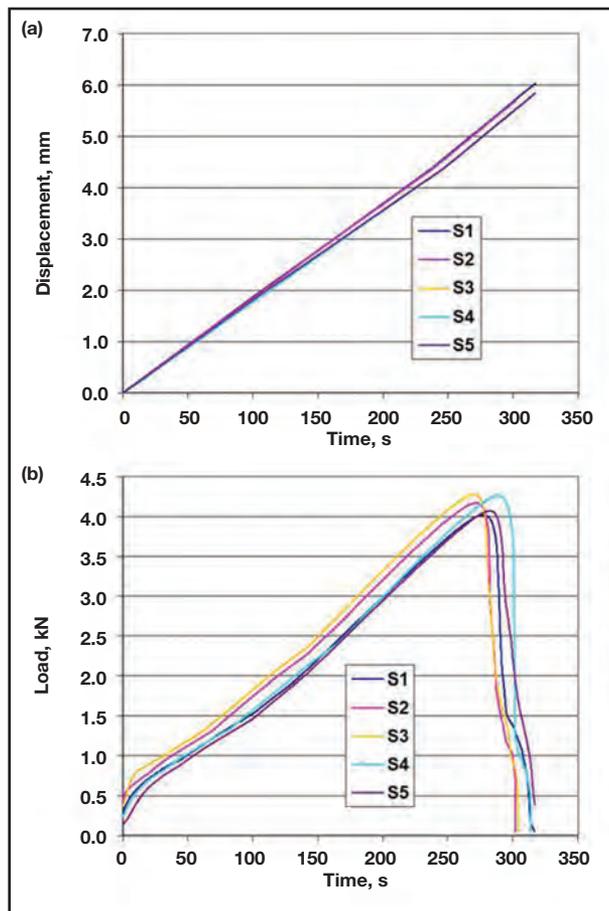


Fig. 6 — Typical static testing results for KSII 90° samples: (a) Displacement and (b) load curve for a spot weld.

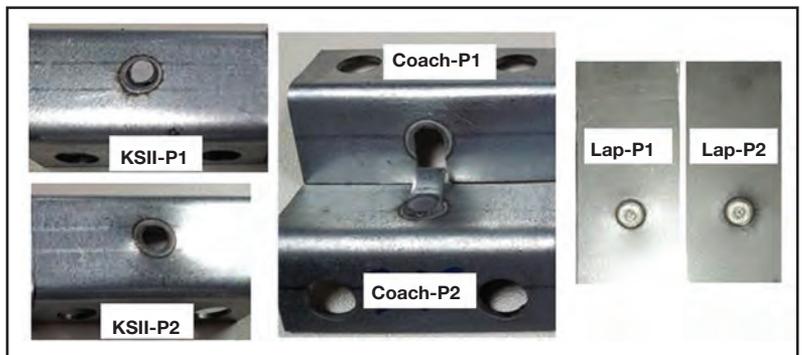


Fig. 7 — Typical broken samples for KSII, coach-peel, and lap-shear testing.



Fig. 8 — Drop tower for high speed sample testing.

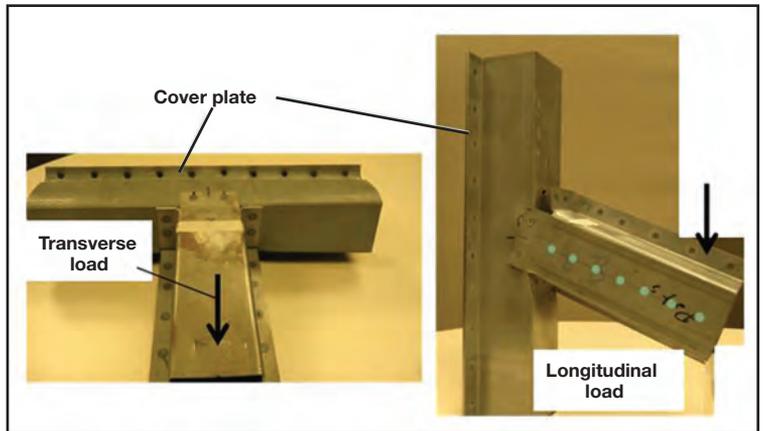


Fig. 9 — Broken T-Section samples.

signed and tested to validate failure parameters at the component level. □

For more information: Yu-Ping Yang is a principal engineer in the structure integrity and modeling group at EWI, 1250 Arthur E. Adams Dr., Columbus, OH 43221, 614.688.5253, yyang@ewi.org, ewi.org.

References

1. S.-H. Lin, et al., A General Failure Criterion for Spot Welds Under Combined Loading Conditions, *Int. J. Solids Struct.*, Vol 40, p 5539-5564, 2003.

2. F. Seeger, et al., An Investigation on Spot Weld Modeling for Crash Simulation with LS-DYNA, 4th LS-DYNA User Forum, Bamberg, Germany, 2005.

3. Y.P. Yang, et al., Integrated Computational Model to Predict Mechanical Behavior of Spot Weld, *Sci. Technol. Weld. Join.*, Vol 13(3), p 232-239, 2008.

4. Y.P. Yang, et al., Development of Spot Weld Failure Parameters for Full Vehicle Crash Modeling, *Sci. Technol. Weld. Join.*, Vol 18(3), p 222-231, 2013.

5. N. Mori, et al., Fatigue Life Prediction Methods for Spot Welds in T-Shaped Members Under Bending, SAE Paper 860604, Warrendale, PA, 1986.

Is your *tired* lever arm tester dreaming of renewal?

Let ATS update your testers with WinCCS Control!

ATS APPLIED TEST SYSTEMS
THE MARK OF RELIABILITY
(724) 283-1212 www.atspa.com sales@atspa.com

Structural Adhesive Resists High Temperatures

Master Bond Supreme 45HTQ

- ◆ Toughened, quartz filled epoxy
- ◆ Serviceable from -60°F to 450°F
- ◆ Superior durability and chemical resistance
- ◆ High compressive strength

MASTERBOND
ADHESIVES | SEALANTS | COATINGS

Hackensack, NJ 07601 USA • +1.201.343.8983
main@masterbond.com

www.masterbond.com